

TASK CLOSE OUT DOCUMENT

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IAG

Task Scope Host level communication  
with legislators

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Task No. 44 Date Complete 4/27/99

Reason felt task is complete:

Estimate made based on 'C' long presentation  
delivered during meeting on 4/27.

Members of Committee

- M. POLAR
- T. KENDALL
- Wanda Stump
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M. C. H. [Signature]  
Signal  
Committee Leader

TASK 46 HEAT LOSSES FROM PRIMARY COOLANT SYSTEM

Purpose:

To determine the time at which no external cooling - other than make up and let-down flow-will be required.

Method:

System heat losses were estimated using the cooldown rate of the "B" hot leg during stratification following the pump trip on 4/27. Let-down flow was estimated using measured flow rates for various pressures. Decay heat was extrapolated from S&W curves.

Conclusions:

- 1) The heat loss with an average  $\Delta T$  of  $100^{\circ}F$  between primary system and containment is about 0.1 M W. + losses through control rod drive penetrations.
- 2) A let-down flow rate of at least 15gpm has been achieved at pressures from about 1000 down to 300 psig. This flow could remove about 0.1mw.
- 3) The decay heat will reach 0.2 mw within a year.



## Heat Losses From System - Hot Leg Piping

Assume that loop B cooldown during 4/28 and 9/29 was with zero flow, rejecting heat to the containment

Assume  $T_{\text{containment}} = 80^{\circ}\text{F}$

With  $T_H^{\circ} = 190^{\circ}\text{F}$   $DT/dt \approx 20^{\circ}\text{F}/35 \text{ hrs} = 571^{\circ}\text{F/hr}$

$$m c_p \frac{dT}{dt} = U A (T - T_{\infty})$$

Pipe Dimensions:  $OD = 36.5/8"$   $t = 3/8"$

$$\rho_{\text{pipe}} = 488 \text{ lbm/ft}^3 \quad c_p = .11 \text{ Btu/lbm}\cdot^{\circ}\text{F}$$

$$M_{\text{pipe}} = \rho A = (488) \pi \left( (21.474)^2 - (18.313)^2 \right) / 144 = 1322.5 \text{ lbm/ft}$$

$$U A = \frac{m c_p \frac{dT}{dt}}{T - T_{\infty}} = \frac{[(1322.5)(.11) + (441.6)(.11)] (571)}{190 - 80} = 3.05 \frac{\text{Btu}}{\text{hr}\cdot^{\circ}\text{F}\cdot\text{ft}}$$

$$U = \frac{3.05}{\pi (36.625)/12} = \boxed{0.318 \frac{\text{Btu}}{\text{hr}\cdot\text{ft}^2\cdot^{\circ}\text{F}}}$$

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## Heat Losses From System - Calculation

Based on estimate of piping heat transfer coefficient, assume this applies to total system, calculate heat loss from piping and major components as function of temperature. From condenser rate of 2 hot leg during stagnation,  $U_{\text{piping}} \approx .32 \text{ Btu/hr-ft}^2\text{-}^\circ\text{F}$  (this neglects internal thermal resistance and is based on area of pipe outer surface).

### 4hr<sup>2</sup> 70<sup>2</sup> Reactor Vessel -

$$\text{Diameter} - D = 15\frac{1}{8}'$$

$$\text{Ht. including bottom hemisphere} \quad H = 25'$$

$$= 2000 \text{ ft}^2$$

$$UA = 640 \text{ Btu/hr-}^\circ\text{F}$$

Steam Generator - H excludes both hemi-heads

$$D = 12' \quad H = 60'$$

$$A = (\pi DH + \pi D^2) 2$$
$$= 5430 \text{ ft}^2 \quad (2715 \text{ ft}^2/\text{leg})$$

$$2004 \quad 300$$

$$UA = 1740 \text{ Btu/hr-}^\circ\text{F}$$

### Hot Leg Piping -

$$L = 138.6' \quad D = 3.5'$$

$$A = \pi DL = 1524 \text{ ft}^2$$

$$UA = 488 \text{ Btu/hr-}^\circ\text{F}$$



### Cold Leg Piping

$$L = 246.4'$$

$$D = 2.75'$$

$$A = \pi DL = 2130 \text{ ft}^2$$

$$UA = 682 \text{ Btu/hr}\cdot\text{°F}$$

Pressurizer - U.S. Nuclear Energy Research Institute

$$D = 8'$$

$$H = 37'$$

$$A = \pi DH + \pi D^2 = 1131 \text{ ft}^2$$

$$UA = 366 \text{ Btu/hr}\cdot\text{°F}$$

	UA (W/hr·°F)	Q (kw) 80°F ambient				
		120	150	200	250	300
Reactor Vessel	690	7.5	13.1	22.5	31.9	41.3
Hot Leg Piping	488	5.7	10.0	17.2	24.3	31.5
Cold Leg Piping	682	8.0	14.0	24.0	34.0	44.0
SGs	1740	20.4	35.7	61.2	86.7	112.2
subtotal	3550	41.6	72.8	124.8	176.8	228.8
PRR	362	4.2	7.4	12.7	18.0	23.3
total		45.9	80.2	137.6	194.9	252.2

note total heat loss (kw) vs temp.

# Making System Heat Removal Capability

For reference: MW → 748 Btu/sec, assume 20°F ΔT

$$W = \frac{948 \text{ Btu/sec} \cdot (7.48 \text{ gal/ft}^3) \cdot (0.5 \text{ ft}^3/\text{min})}{20 \text{ Btu/lbm} \cdot (57.4 \text{ lbm/ft}^3)} = 340 \text{ gpm/MW}$$

$$.5 \text{ MW} \rightarrow 170 \text{ gpm}$$

Letdown Flow - assume  $W \propto \sqrt{P} \Rightarrow W = 140 \sqrt{\frac{P}{150}} = 3.02 \sqrt{P}$

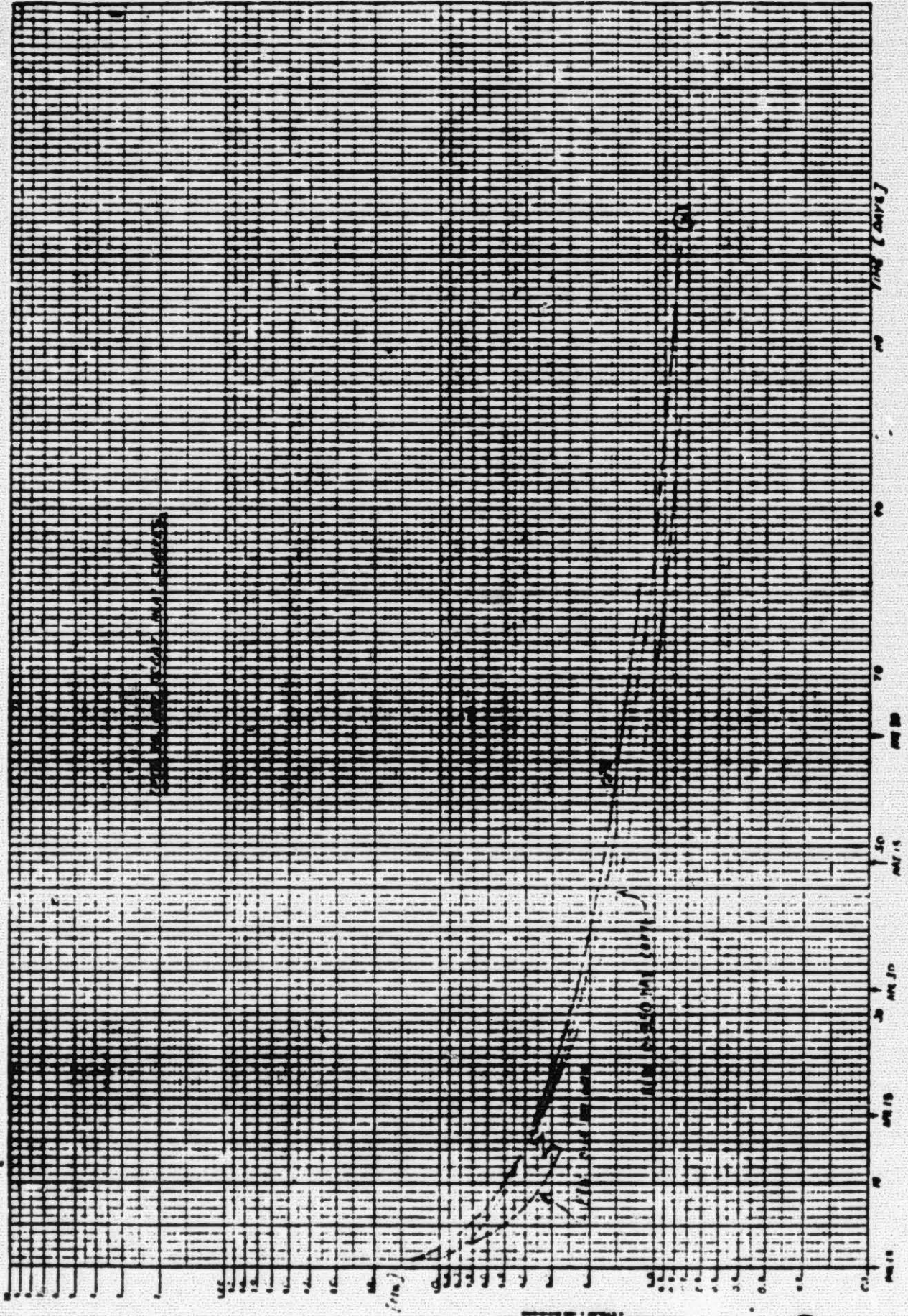
Assume letdown valve can cool return water to 80°F

P (psi)	W (gpm)	Q (MW)		
		T <sub>out</sub> = 100°F	T <sub>out</sub> = 120°F	T <sub>out</sub> = 140°F
300	56.30	.153	.307	.460
200	42.70	.125	.251	.376
100	30.19	.089	.177	.266
50	21.35	.063	.125	.188

$$Q \text{ (MW)} = \frac{W \text{ (gpm)} \times (T_{out} - 80) \text{ Btu/lbm} \cdot (62.4 \text{ lb/ft}^3)}{7.48 \text{ gal/ft}^3 \times 60 \text{ sec/min} \cdot 948 \text{ Btu/MW-sec}} = 1.457 \times 10^{-4} W (T_{out} - 80)$$

Note: This assumes  $W \text{ (gpm)} \propto W_{max} \sqrt{\frac{P}{150}}$ , the dog indicates bypass piping around the pressure breakdown valve (w/ manual valving). If these valves could be opened, a higher flowrate would be available.





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No. 19 19110 107 742 141 18 11 15 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79 80 81 82 83 84 85 86 87 88 89 90 91 92 93 94 95 96 97 98 99 100

100 200 300 400 500 600 700 800 900 1000 1100 1200

System Pressure, Psig

Letdown Flow, gpm

10

20

30

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1200

1000

800

600

400

200

0